

→ Energy Principle

- recall have equation of motion for displacement $\underline{\Sigma}$, in ideal MHD

$$\rho_0 \frac{\partial^2 \underline{\Sigma}}{\partial t^2} = F(\underline{\Sigma})$$

$$\equiv -\hat{L}(\underline{\Sigma})$$

↓
operator (~'spring constant')

Now, \hat{L} self-adjoint, i.e.

$$\int d^3x \vec{\pi} \hat{L}(\vec{\Sigma}) = \int d^3x \vec{\Sigma} \hat{L}(\vec{\Sigma})$$

for any $\vec{\pi}, \vec{\Sigma}$. Proof incorporates B.C.'s.

(see Kadomtsev 159, 160)

Then, can write, for displacement $\underline{\Sigma}$

kinetic energy

$$T = \frac{1}{2} \int_V d^3x \rho_0 \left(\frac{\partial \underline{\Sigma}}{\partial t} \right)^2 \quad (1) \quad (2)$$

potential energy

$$W = \frac{1}{2} \int_V d^3x \left[\gamma \rho_0 (\nabla \cdot \underline{\Sigma})^2 + \frac{1}{4\pi} (\nabla \times \underline{\Sigma} \times \underline{B}_0)^2 \right] \quad (3) \quad (4)$$

" δW "

$$+ \underline{\Sigma} \nabla \rho_0 \nabla \cdot \underline{\Sigma} - \frac{1}{4\pi} [\underline{\Sigma} \times (\nabla \times \underline{B})] \cdot [\nabla \times \underline{\Sigma} \times \underline{B}_0] +$$

⑤

$$\frac{1}{8\pi} \int_{V_e} d^3x (\underline{\nabla} \times \underline{A})^2 - \frac{1}{2} \int dS_o \left(\frac{\partial P_o}{\partial n} + \frac{1}{8\pi} \frac{\partial}{\partial n} \frac{B_o^2}{\epsilon_n} \right.$$

$$\left. - \frac{1}{8\pi} \frac{\partial}{\partial n} B_o^2 \right) \sum_n^2$$

normal displacement

⑥ 193.

① \rightarrow compression

$> 0 \Rightarrow$ always stabilizing.

$$② (\underline{\nabla} \times \hat{\underline{\Sigma}} \times \underline{B}_o)^2 = \left[\underline{B}_o \cdot \underline{\nabla} \hat{\underline{\Sigma}} - \hat{\underline{\Sigma}} \cdot \underline{\nabla} \underline{B}_o - B_o (\underline{\nabla} \cdot \hat{\underline{\Sigma}}) \right]^2$$

(perturbation
magnetic energy)

if $\underline{\nabla} \cdot \hat{\underline{\Sigma}} = 0$, $\begin{cases} \underline{B}_o \text{ uniform} \\ \text{or } \hat{\underline{\Sigma}} \cdot \underline{\nabla} \underline{B}_o = 0 \end{cases}$ then

$$\delta B^2 = (\underline{B}_o \cdot \underline{\nabla} \hat{\underline{\Sigma}})^2 \rightarrow \text{bending energy,}$$

always stabilizing

③ $(\hat{\underline{\Sigma}} \cdot \underline{\nabla} P_o) (\underline{\nabla} \cdot \hat{\underline{\Sigma}}) \rightarrow$ pressure gradient drive

④ $\left[\hat{\underline{\Sigma}} \times (\underline{\nabla} \times \underline{B}_o) \right] \cdot \left[\underline{\nabla} \times \hat{\underline{\Sigma}} \times \underline{B}_o \right] \rightarrow$ kink term
(current gradient)

⑤ \rightarrow gap field energy

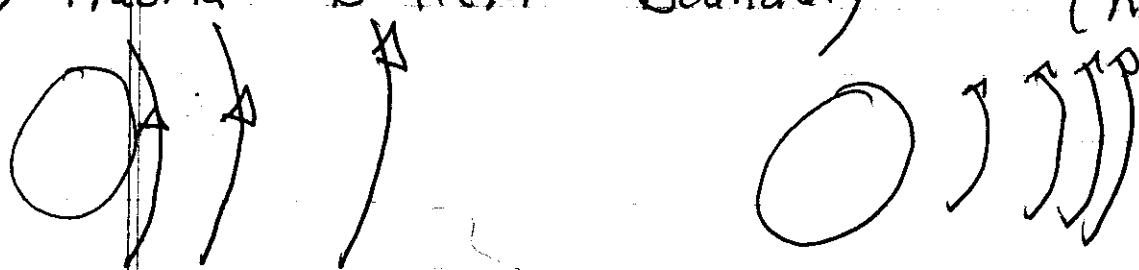
⑥ \rightarrow energy due surface displacement $\frac{\partial}{\partial n} \hat{n} \cdot \underline{\nabla}$

$\int \delta W$

$$\begin{aligned} \frac{dW}{d\delta} > 0 &\rightarrow \text{stable} \\ \frac{dW}{d\delta} < 0 &\rightarrow \text{unstable}. \end{aligned}$$

Some examples: (simple)

a) Plasma - B field Boundary (R.-T.)



$\frac{\partial B_0}{\partial n} \neq 0 \rightarrow \text{unstable}$ $\frac{\partial B_0}{\partial n} > 0 \rightarrow \text{stable}$.

i.e. consider no magnetic field in plasma.

$$B_0 = 0, \text{ flat } p_0$$

$$\therefore \delta W = \frac{1}{2} \int_V d^3x \gamma p_0 (\nabla \cdot \vec{A})^2 + \frac{1}{8\pi} \int_V d^3x (\nabla \times \vec{A})^2 > 0$$

$$+ \frac{1}{16\pi} \int_{S_0} ds \frac{\partial B_0}{\partial n} \sum_n^2 ?$$

For \vec{A} ,

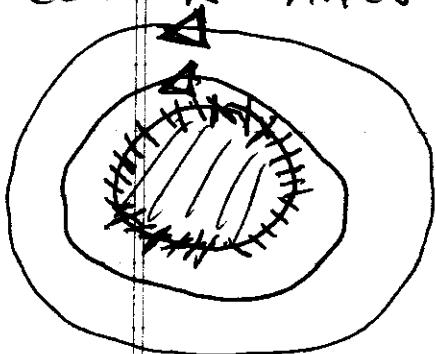
$\frac{\partial B_0}{\partial n} \rightarrow$ field decreases away from plasma boundary
 $\rightarrow \delta W > 0$, so stable.

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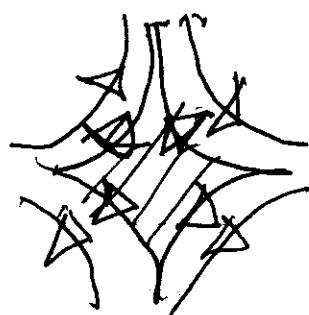
$\frac{\partial B_0}{\partial n} < 0 \rightarrow$ field decreases away from plasma
 \Rightarrow instability !?

i.e.

convex lines (from plasma)



concave lines



(surface current)

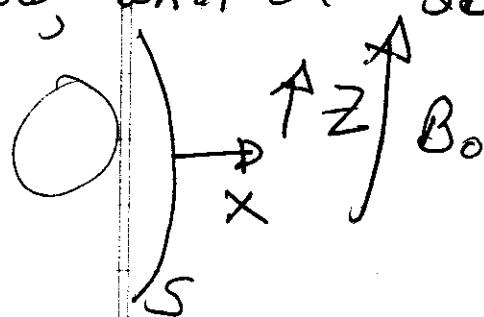
$$\frac{\partial B_0}{\partial n} = 0$$

\rightarrow unstable

$$\frac{\partial B_0}{\partial n} > 0$$

\rightarrow definitely stable

Now, what of $\frac{\partial B_0}{\partial n} < 0 \}$



consider short wavelength perturbation

\Rightarrow surface as planar

$$\therefore E_n = \epsilon_x = \epsilon_0 \exp[ik_y y + ik_z z]$$

Matter inside S conserved $\Rightarrow \underline{D} \cdot \underline{\dot{\epsilon}} = 0$

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now

$$\nabla \times \underline{D} \times \underline{A}_0 = 0$$

$$\nabla(\nabla \cdot \underline{A}_0) - \nabla^2 \underline{A}_0 = 0 \quad k^2 \underline{A}_0 - k(k \cdot \underline{A}_0) = 0$$

and can put $\underline{D} \cdot \underline{A}_0 = 0 \quad (\underline{B} = \underline{D} \times \underline{A}_0)$

$$'' \quad k_x^2 + (k_y^2 + k_z^2) = 0$$

$$\Rightarrow k_x = -c(k_y^2 + k_z^2)^{1/2} = -iR \quad (\text{sw})$$

$$\text{and } \hat{n} \times \hat{\underline{A}} = -\hat{\epsilon}_n B_0 \quad \Rightarrow \begin{aligned} A_{0z} &= 0 \\ A_{0y} &= -\hat{\epsilon}_n B_0 \end{aligned}$$

$$'' \quad |\nabla \times \underline{A}|^2 = 2k_z^2 B_0^2 \epsilon_0^2 e^{-2k_x x}$$

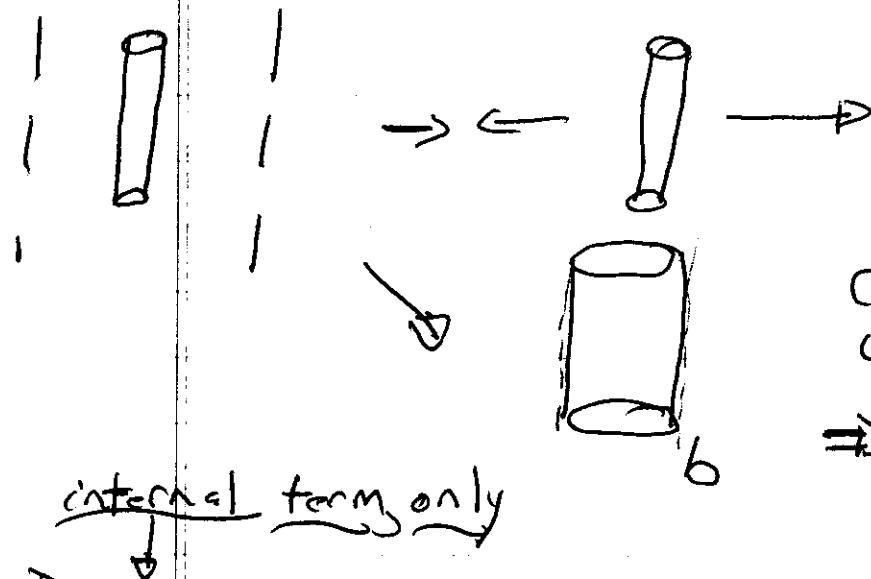
$$'' \quad \Delta W = \int dS \left[\frac{k_z^2 B_0^2}{8\pi R} + \frac{1}{16\pi} \frac{\partial B_0^2}{\partial n} \right] \epsilon_0^2$$

\Rightarrow for $\frac{k_z^2}{R} \rightarrow 0$ (minimal bending)

$\Delta W < 0$ for $\partial B_0^2 / \partial n < 0$.

s.) Pinch - { Distributed Current
{ Localized Modes / Resonant

Now \rightarrow opposite extreme simplification
from surface current pinch



conducting wall
up against plasma
 \Rightarrow no gap, etc.

$$\delta W = \frac{1}{2} \int_V d^3x \left[\gamma \rho_0 (\underline{\nabla} \cdot \underline{\epsilon})^2 + \frac{1}{4\pi} (\underline{\nabla} \times \underline{\epsilon} \times \underline{B}_0)^2 \right]$$

$$+ \underline{\epsilon} \cdot \underline{\nabla} \rho_0 \underline{\nabla} \cdot \underline{\epsilon} - \frac{1}{4\pi} (\underline{\epsilon} \times \underline{\nabla} \times \underline{B}_0) \cdot (\underline{\nabla} \times \underline{\epsilon} \times \underline{B}_0)$$

further, assume cylindrical/helical
symmetry \Rightarrow

$$\underline{\epsilon} = \underline{\epsilon}(r) e^{i(m\theta + k_z z)}$$

\therefore

$$\frac{\delta W}{\delta E_\theta} = 0 \Rightarrow \frac{m}{r} \tilde{E}_\theta + k \tilde{E}_z = \frac{c}{r} \frac{d}{dr} (r \tilde{E}_r)$$

$$\frac{\delta W}{\delta E_z} = 0 \Rightarrow B_z \tilde{E}_\theta - \tilde{E}_z B_\theta =$$

$$\frac{-c}{k^2 r^2 + m^2} \left[(kr B_\theta - m B_z) \frac{d E_r}{dr} \right]$$

$$- (kr B_\theta + m B_z) \frac{E_r}{r} \right]$$

\Leftrightarrow , can eliminate E_θ , E_z and
write (after I. B. P.) :

$$\boxed{\delta W = \frac{\pi}{2} \int_0^b dr \left\{ f \left(\frac{d E_r}{dr} \right)^2 + g E_r^2 \right\}}$$

1D system!

$$f = \frac{n}{4\pi} \frac{(kr B_z + m B_\theta)^2}{k^2 r^2 + m^2} = \frac{n}{4\pi} \frac{(k \cdot B)^2}{(k^2 + m^2/r^2)}$$

$$g = \frac{2k^2 r^2}{k^2 r^2 + m^2} \left(\frac{dP}{dr} \right) + \frac{2n}{4\pi} \frac{(k \cdot B)^2 \left(k^2 + \frac{m^2}{r^2} - 1/r^2 \right)}{(k^2 + m^2/r^2)}$$

$$+ \left(\frac{2k^2 r^3}{4\pi (k^2 r^2 + m^2)^2} \right) \left(k^2 B_z^2 - \frac{k^2 + m^2/r^2}{m^2} B_\theta^2 \right)$$

Now,

$$\frac{\delta W}{\delta \xi_r} = 0 \Rightarrow$$

$$\left. \begin{aligned} & \frac{d}{dr} f \frac{d \xi_r}{dr} - g \xi_r = 0 \\ & \xi_r \Big|_b = 0 \\ & \xi_r \Big|_0 \text{ finite} \end{aligned} \right\} \begin{array}{l} (\text{E.O.M.}) \\ \text{equation} \\ \text{of} \\ \text{motion} \\ \text{for} \\ \text{displacement} \end{array}$$

Now, can further comment:

\rightarrow Full solution is extremum of

$$L = T - W$$

$$\therefore \omega \neq 0 \rightarrow g \rightarrow g + g, \quad \begin{cases} > 0 \text{ for } \omega^2 > 0 \\ < 0 \text{ for } \omega^2 < 0 \end{cases}$$

$$\begin{aligned} L &= +\omega^2 |\ddot{\xi}|^2 - W \\ -L &= W - \omega^2 |\ddot{\xi}|^2 \end{aligned}$$

\oplus extra term

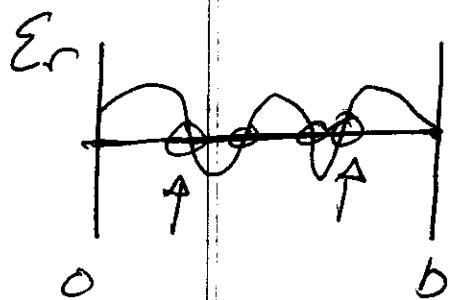
(i.e. $g \neq 0$)

\rightarrow assume solution of E.O.M.

has more than two zeroes in $(0, b)$.

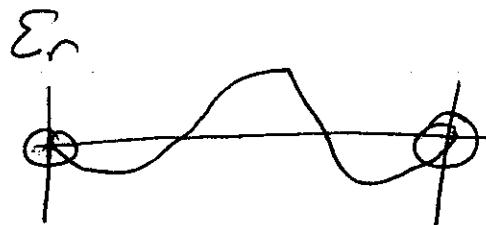
\therefore by adding $g_1 > 0$ ($\Rightarrow \omega^2 < 0$)

can shift zeroes:



\rightarrow adding \oplus to
 $g \Rightarrow$

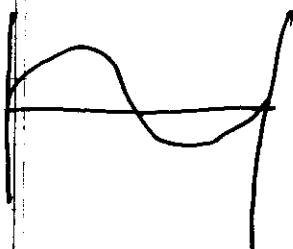
$$\left\{ \begin{array}{l} \frac{d}{dr} f \frac{d}{dr} g E_r = 0 \\ \Rightarrow \text{wiggles less!} \end{array} \right. \quad \begin{array}{l} (\text{wiggles} \Rightarrow) \\ g < 0 \end{array}$$



\Rightarrow modified solution satisfies boundary conditions!

,". corresponds to unstable solution.
 $\omega^2 < 0$.

but if solution F.O.M. has fewer than two zeroes (i.e. 1 zero):



, can only satisfy b.c.'s by wiggling more.

\Rightarrow must add negative g to $g \Rightarrow$
 $\omega^2 > 0$.

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→ Why care about this?

- ⇒ if more than two zeroes in E.O.M. ⇒ instability!
- ⇒ if fewer stability

∴ establishes connection between oscillations/structure of E.O.M. solution and stability.

Implications ⇒

- consider resonant, large m mode
- now, want $dW < 0$ for instability
but: $g = \frac{r(k \cdot B)^2}{4\pi} \frac{\left(k^2 + \frac{m^2}{r^2} - 1\right)}{\left(k^2 + m^2/r^2\right)} + \dots$
- and: $m \rightarrow \infty$
⇒ $k \cdot B$ must $\rightarrow 0$

c.e. only way to reconcile large M and instability is $k \cdot \underline{B} \rightarrow 0$

d.e. mode localized at resonant surface, where $g = m/n$.

$$\text{Now, define } \begin{cases} u = B_\theta / r B_z = \frac{1}{Rg(r)} \\ x = r - r_{m,n} \quad \frac{m}{n} = g(r_{m,n}) \end{cases}$$

so, expanding in x :

$$kr B_z + m B_\theta = m B_z \sin x$$

$\underbrace{}_{\text{Shear}}$

and

$$f = \left(\frac{r^3 B_z^4 k^2}{4\pi B^2} \right) \dot{u}^2 x^2$$

$$g = \frac{2 B_\theta^2}{B^2} \frac{dp}{dr} + \frac{m^2 r B_z^2 \dot{u}^2}{4\pi} x^2$$

\therefore EOM becomes:

$$\frac{d^2 \epsilon_r}{dx^2} + \frac{2}{x} \frac{d\epsilon_r}{dx} + \frac{Q}{x^2} \epsilon_r = K^2 \epsilon_r$$

\Rightarrow where: $Q = -\frac{8\pi\mu^2}{r(\rho)B_z^2} \left(\frac{d\rho_0}{dr} \right)$

$$K^2 = m^2 B^2 / r^2 B_z^2$$

$$\mu' = d\mu/dr$$

Now, obviously RHS negligible
near $x \rightarrow 0$ (i.e. near rational
surface)

$$\therefore \frac{d^2 \epsilon_r}{dx^2} + \frac{2}{x} \frac{d\epsilon_r}{dx} + \frac{Q}{x^2} \epsilon_r = 0$$

$\epsilon_r \sim x^r$, as eqn. homogeneous \Rightarrow

$$\boxed{r = -\frac{1}{2} \pm \sqrt{\frac{1}{4} - Q}}$$

? $\sqrt{\frac{1}{4} - Q} \rightarrow r \text{ real} \rightarrow \text{solutions have}$
no zeroes.

but if $Q > 1/4$

$$\epsilon_r = x^{-1/2} \sin((Q - 1/4)^{1/2} \ln x)$$

∴ infinite # zeroes near $x \rightarrow 0$
 \Rightarrow unstable

Now $Q > 1/4 \Rightarrow$

$$-8\pi r \frac{d\rho}{dr} > \frac{\beta z^2}{4} \left(\frac{d \ln u}{d \ln r} \right)^2$$

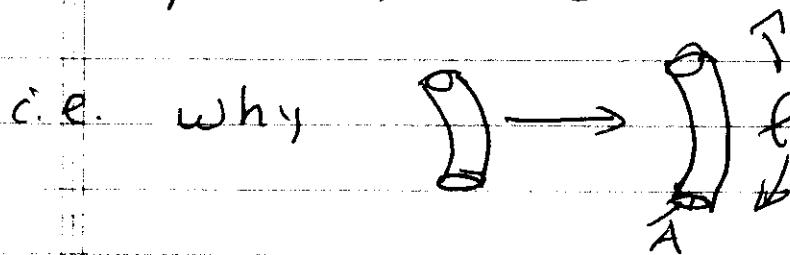
\Rightarrow pressure gradient threshold for instability
 { Suydam Criterion }

- More on Physics of Interchange
(Thermodynamic" Picture of Interchange)
- Can consider interchange of plasma as interchange of flux tubes

i.e.



so, problem that of understanding
why flux tube ① "wants" to
expand from ① → ②



Approach by calculating volume expansion
and extracting force via balance with
PV work.

→ tube "wants" to displace, as will
increase its volume V

i.e. $V = \int A \, dl$
 \downarrow
 cross-sectional area
(flux)

but $\Phi = AB$ is frozen in

so

$$A = \Phi / B$$

and $V = \int dl / B \equiv \Phi / U$

$$U = \int dl / B$$

effective volume, which
tends to increase

- Now, for expansion force \rightarrow effective gravity

$$\rho dV = V F_R dR$$

$$F_R = \left(\frac{dV/dR}{V} \right) \rho \equiv \rho \dot{U} / U$$

effective
force for interchange

$$\boxed{F_R = \rho \dot{U} / U}$$

For simple tokamak

$$U = \int \frac{dl}{B} \sim R^2$$

$$dl \sim R d\phi, \quad B \sim 1/R$$

so,

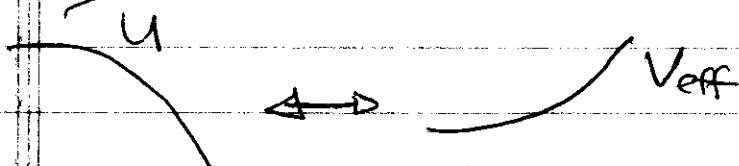
$$\boxed{F_R = 2\rho/R}$$

Note:

- tube expands in direction of increasing $U \Rightarrow -U = V_{\text{eff}}$ - effective potential energy for tube

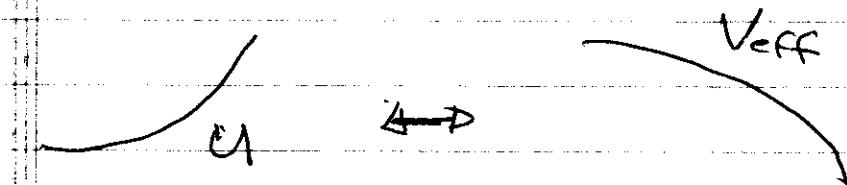
∴

- U decreases from center to edge



\Rightarrow magnetic "well" \rightarrow favorable for stability

- U increases from center to edge



\Rightarrow magnetic hill \rightarrow unfavorable

→ Suydam Done Simply...

Can write reduced MHD equations:

①

$$m_i n_0 \frac{d}{dt} \nabla_{\perp}^2 \phi = \frac{1}{c} (\mathbf{B} \cdot \nabla) J_{||} - \frac{k}{r} \frac{\partial \phi}{\partial \theta}$$

$$\left\{ \begin{array}{l} K \equiv 2B_0^3/r B^2 \sim 1/R_c \quad \text{curvature of field} \\ \text{lines} \\ \text{crucial} - \text{Suydam's stability limit for ideal} \\ \text{interchange.} \end{array} \right.$$

②

$$\text{and } \hat{E}_{||} = 0$$

③

$$\frac{dp}{dt} = 0, \quad \text{as } \nabla \cdot \mathbf{v} = 0$$

So, can immediately write:

$$\begin{aligned} \omega m_i n_0 \nabla_{\perp}^2 \tilde{\phi} &= - \frac{B_0 (m-n_2)}{4\pi r} \nabla_{\perp}^2 \tilde{p} + \frac{m}{rc} \langle J_{||} \rangle' \tilde{\phi} \\ &\quad + \frac{2m}{e^2 R^2} \tilde{p} \end{aligned}$$

$$\omega \tilde{p} = - \frac{B_0 (m-n_2)}{r} \tilde{\phi}$$

$$\omega \tilde{p} = - \frac{m}{r} \tilde{\phi} \langle p' \rangle'$$

so can assemble as:

$$\omega_m, n_0 D_t^2 \left(\frac{\omega \tilde{\psi}}{-\frac{B_0}{r}(m-n\varepsilon)} \right) = -\frac{B_0}{4\pi r} (m-n\varepsilon) D_t^2 \tilde{\psi}$$

$$+ \frac{m}{r c} \langle J_{11} \rangle' \tilde{\psi} + \frac{2m}{\varepsilon^2 R^2} \left(\frac{m}{\omega r} \frac{d\phi}{dr} \right)$$

but $\hat{\phi} = \omega \tilde{\psi} / -\frac{B_0}{r}(m-n\varepsilon)$

$$\omega^2 \left\{ m, n_0 D_t^2 \left(\frac{\tilde{\psi}}{\frac{B_0}{r}(m-n\varepsilon)} \right) \right\} = -\frac{B_0}{4\pi r} (m-n\varepsilon) D_t^2 \tilde{\psi}$$

$$+ \frac{m}{r c} \langle J_{11} \rangle' \tilde{\psi} + \frac{2m}{\varepsilon^2 R^2} \left(\frac{m}{\omega r} \frac{d\phi}{dr} \frac{\omega \tilde{\psi}}{-\frac{B_0}{r}(m-n\varepsilon)} \right)$$

Now if seek determine marginality criterion, take $\omega^2 \rightarrow 0$, so:

$$D_t^2 \tilde{\psi} = \frac{4\pi m}{(m-n\varepsilon)c B_0} \langle J_{11} \rangle' \tilde{\psi} + \frac{8\pi m^2}{B_0^2 (m-n\varepsilon)^2 r} \frac{d\phi}{dr} \tilde{\psi}$$

→ Above is Newcomb Equation → equation

for marginal displacement (i.e. equiv. to
 $\Delta \frac{\partial \bar{P}}{\partial t} = 0 \Rightarrow$ "perturbed eqbm"

Euler eqn) in ideal MHD cis

$$\left\{ \begin{array}{l} \frac{1}{C} (\underline{B} \cdot \nabla) \bar{J}_{||} - \frac{2}{Z^2 R^2} \frac{\partial \bar{P}}{\partial \theta} = 0 \\ \text{with } \underline{B} \cdot \nabla \bar{P} = 0 \end{array} \right.$$

$$\Rightarrow \frac{1}{C} i k_{||} \nabla^2 \tilde{\psi} \underset{①}{\cancel{\frac{C}{4\pi}}} + \frac{1}{C} \tilde{B}_r \frac{\partial \langle \bar{J}_{||} \rangle}{\partial r} \underset{②}{\cancel{- \frac{2}{Z^2 r^2} i m \left(-\frac{\tilde{B}_r}{\tilde{B}_0} \frac{\partial \bar{P}}{\partial k_{||} dr} \right)}} \underset{③}{\cancel{+ 0}}$$

① Current perturbation $\tilde{J}_{||}$

② Displacement of eqbm. current \rightarrow driven currents

③ Curvature driven current ("Pfirsch-Schlüter")
 \rightarrow drives interchanges

→ Obviously, Newcomb equation fails

at $x \rightarrow 0$, unless $\tilde{\psi} \rightarrow 0$, on
 rational surfaces. Need dynamics,

inertia, etc. or $\begin{cases} \text{resistivity} \\ \text{nonlinearity} \dots \end{cases}$

Now:

$$\frac{4\pi m \langle J_{||} \rangle'}{(m-n\Omega) c B_0} = \frac{4\pi m/h \langle J_{||} \rangle'}{(\frac{m-\Omega}{n}) c B_0} = \frac{4\pi \Omega \langle J_{||} \rangle'}{-\Omega' \times c B_0} = \frac{\delta}{X}$$

$$\frac{8\pi m^2}{B^2 (m-n\Omega)^2 r} \frac{dP_0}{dr} = -\frac{\gamma}{X^2}$$

$$\left. \begin{cases} \gamma > 0 \\ \gamma = -\frac{8\pi r dP_0 / dr}{B^2 \Omega'^2} \end{cases} \right\}$$

$$\left. \begin{cases} \delta = n\Omega'/\Omega \\ \text{shear parameter} \\ \Rightarrow \text{rate of pitch rotation.} \end{cases} \right\}$$

have:

$$-\nabla_r^2 \psi + \frac{\delta}{X} \psi - \frac{\gamma}{X^2} \psi = 0$$

as interested in pressure driven modes (i.e. interchanges), take $\delta = 0$.

$$\therefore \left(\nabla_r^2 - \frac{m^2}{r^2} + \frac{\gamma}{X^2} \right) \psi = 0$$

$$kr^2 \gg k_0^2 \Rightarrow \psi \sim X^r$$

$$r(r-1) + \gamma = 0$$

$$\gamma^2 - \gamma + \beta = 0$$

$$\gamma = \frac{1}{2} \pm \frac{1}{2}(1-4\beta)^{1/2}$$

i.e. To avoid instability, need avoid nodes so

$$\beta < 1/4$$

\rightarrow recovery Suydam criterion.

i.e.

$$\left[-\frac{8\pi r}{B^2 S} \frac{dp}{dr} < 1/4 \right] \quad \rightarrow$$

limit on pressure gradient due shear

\rightarrow Physics of Suydam Criterion

Note can write:

$$r \cdot \frac{-dp}{dr} \frac{4\pi}{B^2} < \frac{S^{1/2}}{8}$$

$$\Rightarrow \left\{ \frac{r}{L_p} \beta < \frac{S^{1/2}}{8} = \left(\frac{r_2'}{2} \right)^2 / 8 \right\}$$

$$r_2'/2 = \left(1/L_p^2 \right) (gR)^2$$

$\Rightarrow \beta - \text{limit} > \frac{dp - \text{limit}}{\text{criterion}}$ (in terms stability)

- structurally similar to line-tied inter-change criterion,
i.e. schematically

$$\begin{aligned}\gamma^2 &= \gamma_I^2 - k_{\parallel}^2 V_A^2 \\ &\stackrel{\approx}{=} \frac{k_y^2}{k_{\parallel}^2} \frac{R_c L_0}{\rho_0 dr} C_s^2 - k_{\parallel}^2 V_A^2 \\ &= \frac{C_s^2}{R_c L_0} - k_{\parallel}^2 V_A^2\end{aligned}$$

Now, in sheared system, with resonances

$$k_{\parallel} = \frac{k_0 x}{L_s} \sim \frac{k_0 \Delta x}{L_s}, \quad \begin{cases} \text{IF take } (\Delta x) k_0 \sim 1 \\ \text{i.e. no other scale...} \end{cases}$$

in ideal MHD

$$\gamma^2 = \frac{C_s^2}{R_c L_0} - \frac{V_A^2}{L_s^2}$$

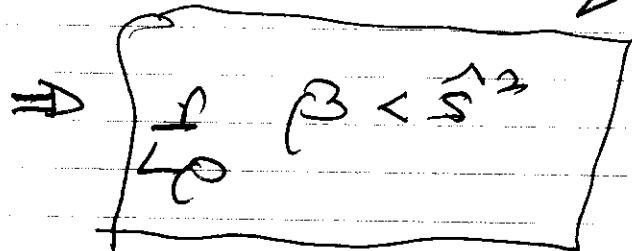
$$\Rightarrow \text{stability for } \frac{(C_s/V_A)^2}{R_c L_0} < \frac{1}{L_s^2}$$

$$\text{if take } 1/L_0 = \tilde{s}/R_L$$

$$\Rightarrow \frac{R_c^2 \tilde{s}^2}{R_c L_0} \beta < \tilde{s}^2$$

but

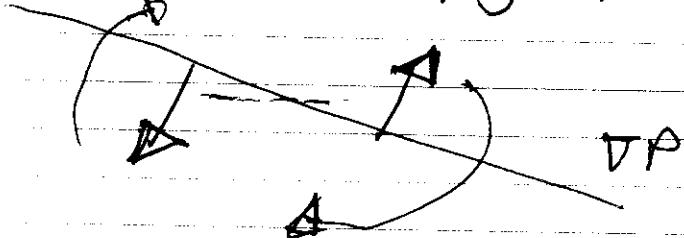
$$1/R_c = \frac{f}{\Omega^2 R^2}$$



\Rightarrow recovers Suydam up to #?

i.e.

- \rightarrow is periodic system with resonances,
shear induces "effective line-tying"¹⁾,
of sorts
- \Rightarrow physics is penalty on energy
to rotate convective cell so that
it is aligned with field.



Stability is gain of gradient relaxation
vs. loss due shear-enforced rotation
penalty.

- \rightarrow "ideal" MHD consistent with
 $k_0 A \sim 1$ choice. Apart from
boundary (excluded here by mode
localization), ideal MHD is scale free,

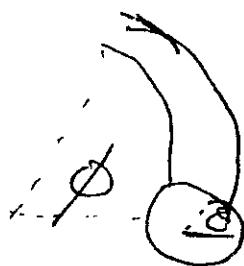
.) Interchange Dynamics in Sheared Magnetic Field

Now in "cylindrical" tokamak:

$$(\epsilon = \alpha/R \ll 1)$$

- $\vec{B}_0 = B_\theta(r)\hat{\theta} + B_z\hat{z}$ $|B_\theta| < B_z$
- periodic perturbations \Rightarrow

$$\hat{\phi} = \sum_{m,n} \hat{\phi}_{m,n} e^{i(m\theta - n\phi)}$$



$$\begin{aligned}\Theta &\equiv \text{poloidal} \\ \phi &\equiv \text{toroidal}\end{aligned}$$

Then, note:

$$\vec{B} \cdot \vec{v} = \frac{B_\theta(r)}{r} \frac{\partial}{\partial \theta} + \frac{B_z}{R} \frac{\partial}{\partial \phi}$$

$$\rightarrow i \left(m \frac{B_\theta(r)}{r} - \frac{n}{R} B_z \right)$$

$$= i \frac{B_z}{R} \left(\frac{m}{Z(r)} - n \right)$$

$q(r) = r B_z / R B_\theta \equiv$ local pitch of magnetic field ("safety factor")

Thus, $k_{\parallel}^{m,n} = \frac{1}{R} \left(\frac{m}{q(r)} - n \right)$

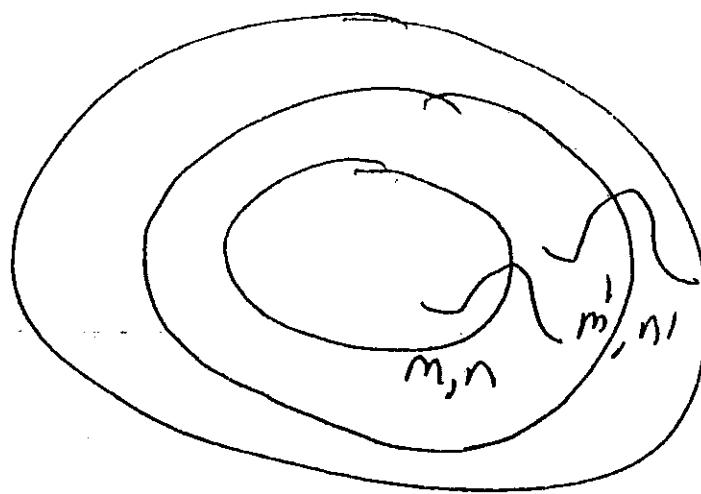
- tends to be small (i.e. line bending, Landau damping, etc. weak) when

$$q(r) = m/n \quad \text{d.e.} \begin{cases} \text{local pitch of field line} \\ = \text{pitch of perturbation} \end{cases}$$

- defines $r_{m,n}$ s.t. $q(r_{m,n}) = m/n$

i.e. $r_{m,n}$ is radius of $\begin{cases} \text{mode rational surface} \\ \text{resonant surface} \end{cases}$ where mode naturally wants to sit, to minimize bending, dissipation etc.

i.e.



Fluctuations
in tokamaks tie
to resonant surf.

natural to write $\hat{\phi}_{m,n} = \hat{\phi}_{m,n}(x)$

where $x = R P_{m,n}$

$$\text{Note: } k_{11} = \frac{1}{R} \left(\frac{m}{I(P_{m,n} + x)} - n \right)$$

$$= \frac{1}{R} \left(-\frac{mg'_{m,n}}{g^2_{m,n}} x \right) + \text{h.o.t.}$$

$$= \frac{k_0 x}{L_s}$$

$$k_0 = m/r$$

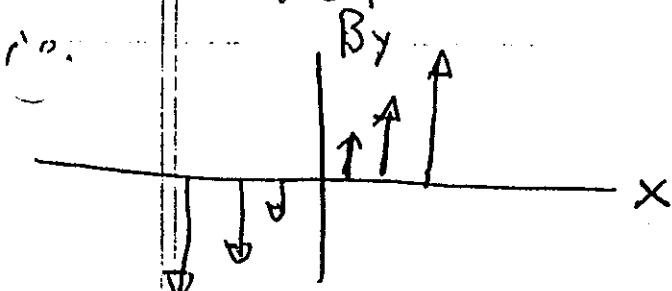
$$\frac{1}{L_s} = -\frac{g'}{R g^2} = \text{magnetic shear length}$$

- equivalent to placing a resonant mode in local field

$$\underline{B} = B_0 \left(\hat{z} + \frac{x}{L_s} \hat{y} \right) \quad \equiv \text{sheared s/cb mode}.$$

Now, can further observe:

- in sheared system, field lines have radially varying orientation



$$B_y = B_0 x / L_s$$

to interchange two flux tubes, need rotate ^(i.e.) frozen-in flux tubes to align (locally) with sheared field

\Rightarrow expect sheared field will exert significant stabilizing effect in ideal interchange.

$$\text{i.e. } \frac{1}{C} \frac{\partial \hat{A}}{\partial t} = \frac{B_z}{4\pi} D_{||} \hat{\phi} \quad , \quad J_z = -D_{\perp}^2 A$$

$$-\frac{\partial^2}{\partial t^2} D_{\perp}^2 \hat{\phi} = \frac{B_0 \cdot \nabla}{\rho_0 c} \frac{\partial J_z}{\partial t} + \frac{\partial^2 \hat{\phi}}{\partial y^2} \frac{g_{\text{eff}}}{L_p}$$

$$\hat{\phi} = \sum_{m,n} e^{i m \omega t} \hat{\phi}_{m,n}(x) e^{i(m\theta - n\phi)}$$

$$+ \gamma \left(\frac{\partial^2}{\partial x^2} - k_\theta^2 \right) \hat{\phi}_{m,n} = + \frac{\gamma B_z k_{||}}{\rho_0 c} \frac{\nabla^2}{\gamma} \left(\frac{\gamma B_z i k_{||}}{4\pi} \hat{\phi}_{m,n} \right)$$

$$+ k_\theta^2 \frac{g_{\text{eff}}}{L_p} \hat{\phi}_{m,n}$$

$$\gamma^2 \left(\frac{\partial^2}{\partial x^2} - k_\theta^2 \right) \hat{\phi}_{m,n} = - V_A^2 k_{||} D_{\perp}^2 (k_{||} \hat{\phi}_{m,n}) + k_\theta^2 \frac{g_{\text{eff}}}{L_p} \hat{\phi}_{m,n}$$

$$\gamma^2 \hat{\phi}_{m,n} = \left[- \frac{k_\theta^2 g_{\text{eff}}}{L_p} \int |\hat{\phi}_{m,n}|^2 dx - V_A^2 \int dx |D_{\perp} k_{||} \hat{\phi}_{m,n}|^2 \right] \frac{1}{\int D_{\perp} \hat{\phi}_{m,n}^2 dx}$$

for scaling:

$$D_1 \sim 1/a \quad (\text{key: No scale for } \vec{\phi}, \text{ other than } a)$$

$$k_{11} \sim \frac{k_0 x}{L_s} \sim \frac{k_0 a}{L_s}$$

so, for β_{crit} (transition to instability):

$$\frac{g_{\text{eff}}}{|L_p|} \geq \frac{V_A^2}{L_s^2} \Rightarrow \frac{L_s^2}{|L_p| R_c} \beta_{\text{crit}} > 1$$

stability if $\beta \leq \frac{|L_p| R_c}{L_s^2} \sim O(\epsilon^2)$ as $L_s \sim R$.

i.e. shear forces / line-tying effect via $D_{11} \rightarrow \sim 1/L_s$.

More detailed analysis confirms basic scaling
 $\beta \leq \frac{|L_p| R_c}{L_s^2}$ (Suydam limit).

Now, useful to consider resistive interchange
 in sheared field

- allows field, fluid to slip (not frozen in!)
- introduces small scale $\Delta x \sim (M/\omega)^{1/2} \ll a$

here, basic smallness parameter is

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$$\frac{1}{S} = \eta/a^2 / V_A/a$$

↓
resistive
diffusion rate

Lundquist #

Alfvén rate

For resistive interchange:

$$-\frac{\partial^2}{\partial t^2} \nabla_{\perp}^2 \vec{\phi} = \frac{B_0 \cdot \nabla}{\rho_0 c} \frac{\partial \hat{J}_z}{\partial t} + \frac{\partial^3 \vec{\phi}}{\partial y^2} \frac{g_{eff}}{4\pi}$$

$$\frac{\partial \hat{J}_z}{\partial t} - \eta \nabla_{\perp}^2 \hat{J}_z = \frac{c}{4\pi} B_0 \cdot \nabla (-\nabla_{\perp}^2 \vec{\phi})$$

Assume $\eta k_{\perp}^2 > \gamma$ (Verify a posteriori!)

$$\Rightarrow \hat{J}_z = + \frac{c}{4\pi} \frac{B_0 \cdot \nabla}{\eta} \vec{\phi}$$

(electrostatic approximation
 i.e. $E_{11} = E_{11}^{inductive} + E_{11,ext}$
 $= n J_{11}$)

$$-\gamma^2 \left(\frac{\partial^2}{\partial x^2} - k_0^2 \right) \vec{\phi} = \frac{\chi_i B_0 k_{11}}{\rho_0 c M} \frac{B_0 k_{11}}{4\pi} \vec{\phi} - k_0^2 g_{eff} \frac{\vec{\phi}}{4\pi}$$

$$\rightarrow \left(\frac{\partial^2}{\partial x^2} - k_0^2 \right) \vec{\phi} - \frac{k_{11}^2 V_A^2}{\gamma M} \vec{\phi} - \frac{k_0^2 g_{\text{eff}}}{L_0^2 \gamma^2} \vec{\phi} = 0$$

$$k_{11} = k_0 x / L_0$$

\Rightarrow Eigenvalue problem for $\gamma_{m,n}$:

$$\left(\frac{\partial^2}{\partial x^2} - k_0^2 \right) \vec{\phi}_{m,n} - \frac{k_0^2 V_A^2}{L_0^2 \gamma M} x^2 \vec{\phi}_{m,n} - \frac{k_0^2 g_{\text{eff}}}{\gamma^2 L_0} \vec{\phi}_{m,n} = 0$$

$$\text{Now, } \vec{\phi}_{m,n} = e^{-\alpha_{m,n} x^2/2} \quad \alpha_{m,n} \sim 1/(\Delta x_{m,n})^2$$

\rightarrow "Slow" interchange ($k_0 \Delta x \ll 1$)

$$\alpha^2 x^2 - \alpha - \frac{k_0^2 V_A^2 x^2}{L_0^2 \gamma M} - \frac{k_0^2 g_{\text{eff}}}{\gamma^2 L_0} = 0$$

$$\alpha = \left(\frac{k_0^2 V_A^2}{L_0^2 \gamma M} \right)^{1/2} \rightarrow \text{defines basic mode scale} \\ (\eta \text{ dependent}, \gamma \text{ dependent})$$

$$\alpha = \frac{k_0^2 g_{\text{eff}}}{\gamma^2 k_0} \rightarrow \text{dispersion relation (need } g_{\text{eff}}/L_0 < 0)$$

To determine γ, α explicitly:

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$$\left(\frac{k_0^2 V_A^2}{L_s^2 \gamma \eta} \right)^{1/2} = \frac{k_0^2}{\gamma^2 L_s} \sigma_{\text{eff}}$$

$$\Rightarrow \gamma = \left(\frac{L_s^2}{L_p^2} \left(\eta k_0^2 \left(\frac{V_A^2}{R_U^2} \right) \beta^2 \right)^{1/3} \right)^{1/3}$$

$\frac{\delta_0}{2}$

$$\left\{ \begin{array}{l} \alpha = \left(\frac{k_0^2 V_A^2}{L_s^2} \left(\frac{L_s^2}{L_p^2} \eta k_0^2 \frac{V_A^2}{R_U^2} \beta^2 \right)^{1/3} \eta \right)^{1/2} \\ \Delta X = 1/\sqrt{\alpha} \end{array} \right.$$

For validity:

$$\left\{ \begin{array}{l} \frac{\eta}{(\Delta X)^2} = \eta \alpha > \gamma \\ k_0^2 (\Delta X)^2 = \frac{k_0^2}{\gamma} < 1 \end{array} \right.$$

\Rightarrow for e.g.:

$$\eta^2 \frac{k_0^2 V_A^2}{L_s^2 \gamma \eta} > \gamma^2$$

$$\gamma \frac{k_0^2 V_A^2}{L_s^2} > \gamma^3 = \frac{L_s^2}{L_p^2} \frac{\gamma}{k_0} \frac{V_A^2}{R_U^2} \beta^2$$

i.e. Need : $\frac{\beta L_s^2}{1/L_p R_c} \ll 1$ for validity of electrostatic approximation.

Note:

i.) $R_c \approx \gamma \Rightarrow$
m/rankos

$$\gamma \sim \left(\frac{L_s^2 m^2 \beta^2}{4 \rho^2} \right)^{1/3} \left(\frac{V_A^2}{a^2} \frac{V_A^2}{a^2} \right)^{1/3}$$

$$\sim (1/R T_A)^{1/3} \Rightarrow \gamma T_A \sim S^{-1/3} \beta^{2/3} (k_B/T_p)$$

i.e. growth rate is hybrid of resistive diffuser and Alfvén rates

\Rightarrow resistive diffusion allows decoupling of field, fluid, thereby triggering instability.

ii.) For incompressible MHD, have instability for all β (i.e. unlike ideal MHD, no β_{crit} exists!)

$$\text{i.) } \Delta x = \left(L_s^2 \gamma A / k_B V_A^2 \right)^{1/4} \ll a \\ \sim S^{-1/3} \beta^{1/6}$$

i.e. $\Delta x/a \sim S^{-1/3} \xrightarrow{\beta} \text{narrow layer.}$

(ii) For fast interchange: $k_0^2(\Delta x)^2 > 1$

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Thus, as before:

$$\frac{\omega^2 X^2}{2} - \alpha - k_0^2 - \frac{k_0^2 V_A^2 X^2}{4\omega^2 \gamma m} - \frac{g_{\text{eff}} k_0^2}{\gamma^2 L_D} = 0$$

$$\Rightarrow \alpha = \left(\frac{k_0^2 V_A^2}{4\omega^2 \gamma m} \right)^{1/2}$$

$\frac{k_0^2}{2} > 1 \Rightarrow$ now obtain dispersion relation:

$$-\frac{\omega^2}{k_0^2} = -\frac{g_{\text{eff}} k_0^2}{\gamma^2 L_D}$$

$$\gamma^2 = g_{\text{eff}} / |L_D| = c_s^2 / R_{\text{eff}} |L_D|$$

$$\Delta x \sim S^{-1/2}$$

Note:

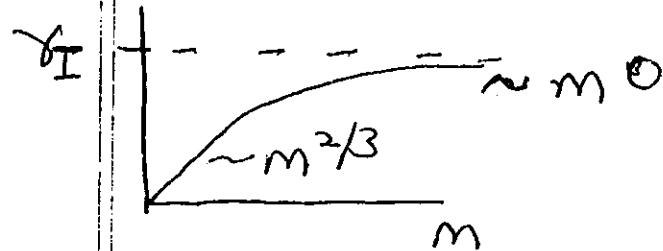
(i) Fast regime entered when:

$$\frac{k_0^2}{2} > 1 \Rightarrow \frac{k_0^2}{\left(\frac{k_0^2 V_A^2}{4\omega^2 \gamma m} \right)^{1/2}} > 1$$

$$k_0^2 > \frac{k_0^2 V_A^2}{4\omega^2 \gamma m}$$

$$\eta k_0^2 > V_A^2 / L_s^2 \gamma_I$$

i.e. fast interchange dominates at large m



In practice, large η or high $m \Rightarrow$ fast interchange

(i.) Note essence of fast interchange is:

- high ηk_0^2
- ideal growth rate.

Physical content is that ηk_0^2 so large that line-bending destroyed and mode reverts to ideal growth

(ii.) Note $\Delta x \sim \delta'^{-1/2}$ i.e. mode still localized by η . also $\delta \Delta^2 \sim \eta$

(iv.) In reality, fast interchange even fully cut-off by dissipation (μ_j , etc.).

v.) All resistive interchanges localized to $B_0 = 0$ resonant surfaces.