


→ Schematic Notes on Quasi-Modes

→ Should be read as Supplement to   
Roberts-Taylor Paper

# i.) Quasimodes and Relation to Resistive Interchanges

Ref.: K.V. Roberts and J.B. Taylor, Phys. Fluids 8 315 (1965).

→ Note: Salient features of resistive interchange

- localized to  $\Delta/a \sim S^{-1/3}$  of  $\underline{k} \cdot \underline{B}_0 = 0$  surface
- mode tied to resistive layer  $\Delta/a \sim S^{-1/3}$

Contrast: Ideal interchange (shear-free system)

- global mode  $\Delta/a \sim k_x a \sim 1$
- no special preferred location

→ Motivation:

- instabilities of interest due to transport caused (i.e. effect on confinement)
- mode space and time scales determine transport

$$D \sim (\Delta x)^2 / \tau_c \sim \gamma / k_x^2$$

- for resistive g-mode  $k_x \sim \Delta^{-1} \sim S^{-1/3}$

$$D \sim \gamma / k_x^2 \sim \eta \beta$$

↓

global transport on resistive diffusion timescale (slow)

- thus, natural to seek resistive modes / wave-packets with  $k_x a \sim 1$  (larger transport)

- intuition is that may be able to construct quasi-mode wave-packets with  $\gamma \sim \eta^{1/3}$ ,  $k_x a \sim 1$  i.e. radial structure of resistive-interchange determined by fourier analysis, as well as physics.

→ Approach:

- Consider sequence of small problems:

① ideal interchange + resistively coated end plates (localized resistivity ⇔ no line tying)

⇒ interchanging tubes can rotate, to adjust locally to shear

② distributed  $\eta$ , line-tying but no shear

⇒  $\eta$  allows growing "shearing modes", with

$$\gamma \sim \eta k_y^2 \frac{g/L_p}{k_{ii}^2 v_A^2}$$

③ distributed  $\eta$ , no line-tying but finite shear

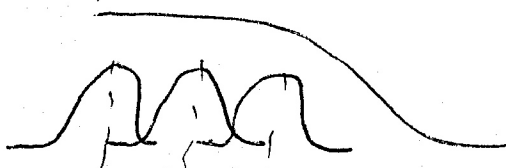
$\Rightarrow$  finite length (along  $B_0$ ) wave-packet, with  $k_x a \sim 1$ . Here,

$$\gamma \sim \eta k_y^2 \frac{\gamma_I^2 L^2}{v_A^2}$$

with  $L \eta^{-1/3} \Rightarrow$  recovers  $\gamma \sim \eta^{1/3}$

$\Rightarrow$  wave packet is superposition of localized g-modes with approximately identical growth rates.

ie.



$k_x \cdot \underline{D} = 0$   $k_y \cdot \underline{D} = 0$   $\Rightarrow$  local orientation twists to align with shear

① Ideal Interchange with resistively coated plates



Recall, for ideal interchange

$$\gamma^2 \nabla_{\perp}^2 \vec{\phi} = V_A^2 \nabla_{\parallel} \nabla_{\perp}^2 \nabla_{\parallel} \vec{\phi} + \frac{g}{4\pi} \frac{\partial^2}{\partial y^2} \vec{\phi}$$

$$\nabla_{\parallel} = \frac{\mathbf{k} \cdot \mathbf{B}_0}{|\mathbf{B}_0|} \rightarrow k_y \frac{x}{L_s}$$

$$\nabla_{\parallel} = \left( \frac{\partial}{\partial z} + \frac{x}{L_s} \frac{\partial}{\partial y} \right)$$

After to use "twisting coordinates": (aligned with shear)

$$\xi = x \quad d\xi = dx$$

$$\chi = y - \frac{x}{L_s} z \quad d\chi = dy - \frac{1}{L_s} (x dz + z dx)$$

$$\varphi = z \quad d\varphi = dz$$

$$\frac{\partial}{\partial z} = \frac{d\chi}{dz} \frac{\partial}{\partial \chi} + \frac{d\xi}{dz} \frac{\partial}{\partial \xi} + \frac{d\varphi}{dz} \frac{\partial}{\partial \varphi}$$

$$= -\frac{x}{L_s} \frac{\partial}{\partial \chi} + 0 + \frac{\partial}{\partial \varphi}$$

$$\partial/\partial y = \partial/\partial \chi$$

⇒

$$\frac{\partial}{\partial z} + \frac{x}{L_0} \frac{\partial}{\partial y} = \frac{\partial}{\partial \varphi}$$

⇒

$$\gamma^2 \nabla_1^2 \phi = v_A^2 \frac{\partial}{\partial \varphi} \nabla_1^2 \frac{\partial}{\partial \varphi} \phi + \frac{g}{|k_\perp|} \frac{\partial^2}{\partial \chi^2} \phi$$

$$\phi = \phi^{(0)} + \phi^{(1)} + \dots$$

$$k_\perp^2 v_A^2 \gg \gamma_I^2 \gg \gamma^2$$

⇒

$$v_A^2 \frac{\partial}{\partial \varphi} \nabla_1^2 \frac{\partial}{\partial \varphi} \phi^{(0)} = 0$$

$$\Leftrightarrow D_0 \phi^{(0)} = 0$$

$$\gamma^2 \nabla_1^2 \phi^{(1)} = v_A^2 \frac{\partial}{\partial \varphi} \nabla_1^2 \frac{\partial}{\partial \varphi} \phi^{(1)} + \frac{g}{|k_\perp|} \frac{\partial^2}{\partial \chi^2} \phi^{(0)}$$

⇔

$$D_0 \phi^{(1)} = D_1 \phi^{(0)}$$

solvable only if  $\int_{-L}^L \phi^{(0)} D_1 \phi^{(0)} d\varphi = 0$

- Igebrn  $\Rightarrow$

$$\frac{d^2 \phi^{(q)}}{d\Sigma^2} + (A \Sigma^2 + B) \phi^{(q)} = 0$$

$$A = \frac{k_y^2}{L_s^2} \left( \frac{g}{4\gamma^2} - 1 \right)$$

$$B = k_y^2 \left( \frac{g}{4\gamma^2} - 1 - \frac{L^2}{3L_s^2} \right)$$

$\phi = 0$  at  $x = \pm H \Rightarrow \frac{1}{\phi^{(q)}} \frac{d^2 \phi^{(q)}}{d\Sigma^2} < 0$

$\Rightarrow \left( \frac{\gamma_{II}^2}{\gamma^2} - 1 \right) > \frac{1}{3} \frac{L^2}{L_s^2} / \left( 1 + \frac{H^2}{L^2} \right)$

i.e

-  $L_s$  slows interchange growth, but does not stabilize interchange

$\downarrow$

- consequence of resistivity localized to end plates

(2) Shear-Free + Line-Tying

Recall :

$$-\phi \sim \cos \frac{m\pi z}{2L} \sin \frac{n\pi x}{2H} e^{ik_y y} \quad (\text{h.c.'s})$$

⇒

$$\gamma^2 + \frac{k_z^2 V_A^2 \gamma}{\gamma + \eta k_\perp^2} - \frac{g k_y^2}{|k_\perp|^2} = 0 \quad (\text{local dispn.})$$

$$k_\perp^2 = k_x^2 + k_y^2$$

Now, consistent with motivation:

$$- k_x \ll k_y \Rightarrow k_\perp \approx k_y$$

$$- k_z \approx \pi/L$$

Further:

$$- \eta k_\perp^2 > \gamma$$

$$- k_z^2 V_A^2 \gg \gamma \eta k_y^2$$

(but  $\eta k_y^2$  finite  $\Rightarrow \gamma \neq k_\perp^2$ )

⇒

$$\gamma^2 + \frac{k_z^2 V_A^2 \gamma}{\eta k_y^2} - \frac{g}{|k_\perp|} = 0$$

∴

$$\gamma \approx \frac{\gamma_I^2 \eta k_y^2}{k_z^2 V_A^2}$$

$$\approx \gamma_I^2 \eta k_y^2 \frac{L^2}{V_A^2}$$

↑  
system length

Note:

-  $\gamma$  independent  $k_x$ , and  $\sim k_y^2$  (but  $\gamma \sim \gamma_I$  as  $\eta k_y^2 \rightarrow \infty$ ).

- rapid variation is in  $y \Rightarrow$  modes slice, so alternate layers parallel to  $B_0$  move up and down. Growth bigger for smaller slice.

- growth depends on  $\eta L^2$  (system length appears)  $\Rightarrow$  reflects fact that energy into bent field lines

$$-\gamma \frac{dn}{n} = -\frac{\hat{V}_r}{L_p} = \frac{\gamma \hat{\Sigma}}{L_p}$$

$$\hat{\Sigma} = \frac{dn}{n} L_p \quad \Rightarrow \text{vertical } (\hat{x}) \text{ displacement related to } dn/n$$

Now, approximate equilibrium if:

-  $\delta x = \frac{\gamma_I^2 L_0}{k_z^2 V_A^2} \rightarrow$  i.e. displacement of  $B_0$  for local eq. brm

but bending  $B_0 \Rightarrow \tilde{B}_\perp$ . When dissipated, <sup>( $\eta!$ )</sup> growth can proceed  $\Rightarrow$

$$\frac{1}{\delta x} \frac{d\delta x}{dt} = \left( \frac{\gamma_I^2}{k_z^2 V_A^2} \right) \frac{\eta k_y^2}{L} \Rightarrow \text{basic growth scaling!}$$

↓  
diss. rate

i.e. resistive diffusion destroys 'line-tied' equilibrium!

○ Finite Shear, no line-tying

$$\nabla_\perp^2 \hat{\phi} + \frac{V_A^2}{\delta \eta} \nabla_{||}^2 \hat{\phi} + \frac{g}{k_0 \delta^2} k_y^2 \hat{\phi} = 0$$

in twisting coordinates:  $\begin{cases} x = y - \frac{\chi}{L_0} z \\ z = z \\ y = y \end{cases}$

$$\nabla_{||} \rightarrow \frac{\partial}{\partial \varphi}$$

$$\nabla_\perp^2 = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2}$$

$$\frac{\partial}{\partial y} = \frac{d\chi}{dy} \frac{\partial}{\partial y} + \frac{d\chi}{dy} \frac{\partial}{\partial x} + \frac{\partial \phi}{\partial y} \frac{\partial}{\partial \varphi} = \frac{\partial}{\partial x}$$

$$-\frac{\partial}{\partial x} = \frac{d\Sigma}{dx} \frac{\partial}{\partial \Sigma} + \frac{d\chi}{dx} \frac{\partial}{\partial \chi} + \frac{d\psi}{dx} \frac{\partial}{\partial \psi}$$

$$= \frac{\partial}{\partial \Sigma} - \frac{z}{L_0} \frac{\partial}{\partial \chi}$$

$$= \frac{\partial}{\partial \Sigma} - \frac{\varphi}{L_0} \frac{\partial}{\partial \chi}, \text{ in twisting coords.}$$

$\Rightarrow$

$$\left[ \left( \frac{\partial}{\partial \Sigma} - \frac{\varphi}{L_0} \frac{\partial}{\partial \chi} \right)^2 + \frac{\partial^2}{\partial \chi^2} \right] \hat{\phi} + \frac{V_A^2}{\gamma_1} \frac{\partial^2 \hat{\phi}}{\partial \psi^2}$$

$$- \frac{g}{4\pi \gamma_1 \delta^2} \frac{\partial^2 \hat{\phi}}{\partial \chi^2} = 0$$

$$\hat{\phi} = e^{ik_x \Sigma} e^{ik_y \chi} \hat{\phi}(\psi)$$

$$= e^{ik_x X} e^{ik_y (y - \frac{z}{L_0} z)} \hat{\phi}(z)$$

$\Rightarrow$

$\hookrightarrow$  {eigenfunction describes length along field line

$$- \left[ \left( k_x - \frac{k_y \varphi}{L_0} \right)^2 + k_y^2 \right] \hat{\phi} + \frac{V_A^2}{\gamma_1} \frac{\partial^2 \hat{\phi}}{\partial \psi^2} + \frac{k_y^2 g}{4\pi \delta^2} \hat{\phi} = 0$$

$$\frac{\partial^2 \hat{\phi}}{\partial \psi^2} - \frac{\gamma_1 k_y^2}{V_A^2} \left[ \left( \frac{k_x}{k_y} - \frac{\varphi}{L_0} \right)^2 + 1 \right] \hat{\phi} + \frac{k_y^2 g \gamma_1}{4\pi V_A^2 \delta^2} \hat{\phi} = 0$$

if  $k_x \ll k_y \Rightarrow$

$$\frac{\partial^2 \vec{\phi}}{\partial \varphi^2} - \frac{\gamma \eta k_y^2}{V_A^2} \left[ \frac{\varphi^2}{L_S^2} + 1 \right] \vec{\phi} + \frac{\eta k_y^2 \gamma_I^2}{\gamma V_A^2} \vec{\phi} = 0$$

$$\vec{\phi}(\varphi) = e^{-\alpha \varphi^2 / 2}$$

$$\partial^2 \varphi^2 - \alpha - \frac{\gamma \eta k_y^2}{V_A^2 L_S^2} \varphi^2 - \frac{\gamma \eta k_y^2}{V_A^2} + \frac{\eta k_y^2 \gamma_I^2}{\gamma V_A^2} = 0$$

( $\alpha^2 > L_S^2$ )

$$\alpha = \left( \frac{\gamma \eta k_y^2}{V_A^2 L_S^2} \right)^{1/2}$$

$$\left( \frac{\gamma \eta k_y^2}{V_A^2 L_S^2} \right)^{1/2} = \frac{\eta k_y^2 \gamma_I^2}{\gamma V_A^2}$$

$$\Rightarrow \left\{ \begin{array}{l} \gamma V_A \sim \eta^{-1/3}, \quad \gamma \sim \eta^{1/3} \\ \sqrt{\alpha} \sim 1/L_{\text{eff}} \sim \eta^{1/3} \quad \Rightarrow L_{\text{eff}} \sim \eta^{-1/3} \end{array} \right.$$

Note:

- as all dynamics independent of  $k_x$ , can take  $k_x a \sim 1$  and



$$\phi = F(x) \hat{\phi}(z) e^{iky(y - \frac{x}{L_0} z)}$$

$$\downarrow \quad \downarrow$$

arbitrary envelope in  $x$ ,  
 slowly varying in comparison  $k_y$

$$\hat{\phi}(z) \text{ eigenfunction } L \sim \eta^{-1/3}$$

- "modes" are finite length rolls, locally aligned with shear:

i.e. pattern  $\phi$  constant along  $y - \frac{xz}{L_0} \equiv \text{const.}$

- "modes" have finite length in  $z$  (allow twist to align with shear).

-  $\gamma \sim \eta^{1/3}$  but  $k_x a \sim 1 \Rightarrow$  large transport

- can derive from local analysis with  $L \sim \eta^{-1/3}$   
 i.e. energetics determine length (must keep rotation energy finite)

- "modes" are really wave-packets of localized  $g$ -modes

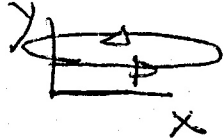
$$\text{i.e. } k_{in} = \frac{k_y x}{L_0} \quad \left( e^{ik_{in} x} \right) \rightarrow \frac{\partial}{\partial L} \left. \begin{array}{l} \text{"radial and"} \\ \text{"along field"} \\ \text{spaces} \\ \text{reciprocal} \end{array} \right\}$$

$$\frac{\partial}{\partial x} = \frac{k_y}{L_0} \frac{\partial}{\partial k_{in}} \quad \rightarrow \frac{k_y L}{L_0}$$

with length  $\leftrightarrow$  envelope !

key point is insensitivity to  $x$  variation ( $\sim$  const profile) allows superposition, s/t :

-  $k_x \ll k_y$



- natural for growth (large step)

$\Rightarrow$  dynamically favored

i.e. localization in  $\hat{x}$  is consequence Fourier analysis, not physical nature of disturbance !!

- in nonlinear regime: (P)

- packets may fall apart

-  $k \cdot \nabla' x z \rightarrow \frac{k_y k_y'}{L_s} z (x - x') = 0$

coupling ?

- sub-scale instability

